#### Nicolas BORGHINI

Dissipative effects in heavy ion collisions

Principle and ideas of the calculations

Results

#### Christian Lang & N.B., arXiv:1312.???

New frontiers in QCD, YITP, Kyoto, Nov.-Dec., 2013

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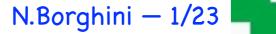


#### Dissipative effects in heavy ion collisions

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When going from ideal fluid dynamics to dissipative fluid dynamics, the corrections (viscosity, (heat conductivity), ...) are twofold:

 $\boldsymbol{\textit{o}}$  modification of the fluid four-velocity  $u(\boldsymbol{x})$ 

**r** solution of 
$$\partial_{\mu}T^{\mu\nu}(\mathbf{x}) = 0$$
 with

$$T^{\mu\nu}(\mathbf{x}) = \epsilon(\mathbf{x})u^{\mu}(\mathbf{x})u^{\nu}(\mathbf{x}) - \mathcal{P}(\mathbf{x})\Delta^{\mu\nu}(\mathbf{x}) + \pi^{\mu\nu}(\mathbf{x})$$

🤪 at freeze-out

within the (naive?) Cooper-Frye prescription

$$E_{\vec{p}} \frac{\mathrm{d}^3 N}{\mathrm{d}^3 \vec{p}} = \frac{g}{(2\pi)^3} \int_{\Sigma} f\left(\frac{\mathbf{p} \cdot \mathbf{u}(\mathbf{x})}{T}\right) \mathbf{p} \cdot \mathrm{d}^3 \sigma(\mathbf{x})$$

freceives corrections  $f = f_{id.} + \delta f^{(1)} + \delta f^{(2)} + \cdots$  so that  $T^{\mu\nu}$  remain continuous in the transition from a fluid to a collection of particles.

When going from ideal fluid dynamics to dissipative fluid dynamics, the corrections (viscosity, (heat conductivity), ...) are twofold:

 $\boldsymbol{\textit{o}}$  modification of the fluid four-velocity  $u(\boldsymbol{x})$ 

resolution of 
$$\partial_{\mu}T^{\mu\nu}(\mathbf{x}) = 0$$
 with

$$T^{\mu\nu}(\mathbf{x}) = \epsilon(\mathbf{x})u^{\mu}(\mathbf{x})u^{\nu}(\mathbf{x}) - \mathcal{P}(\mathbf{x})\Delta^{\mu\nu}(\mathbf{x}) + \pi^{\mu\nu}(\mathbf{x})$$

The dissipative part  $\pi^{\mu\nu}$  of the stress tensor involves the various transport coefficients ( $\eta$ ,  $\zeta$ ,  $\kappa$ ...).

Here, the temperature dependences of the coefficients over the whole history of the hydrodynamical evolution affect the particle spectra.

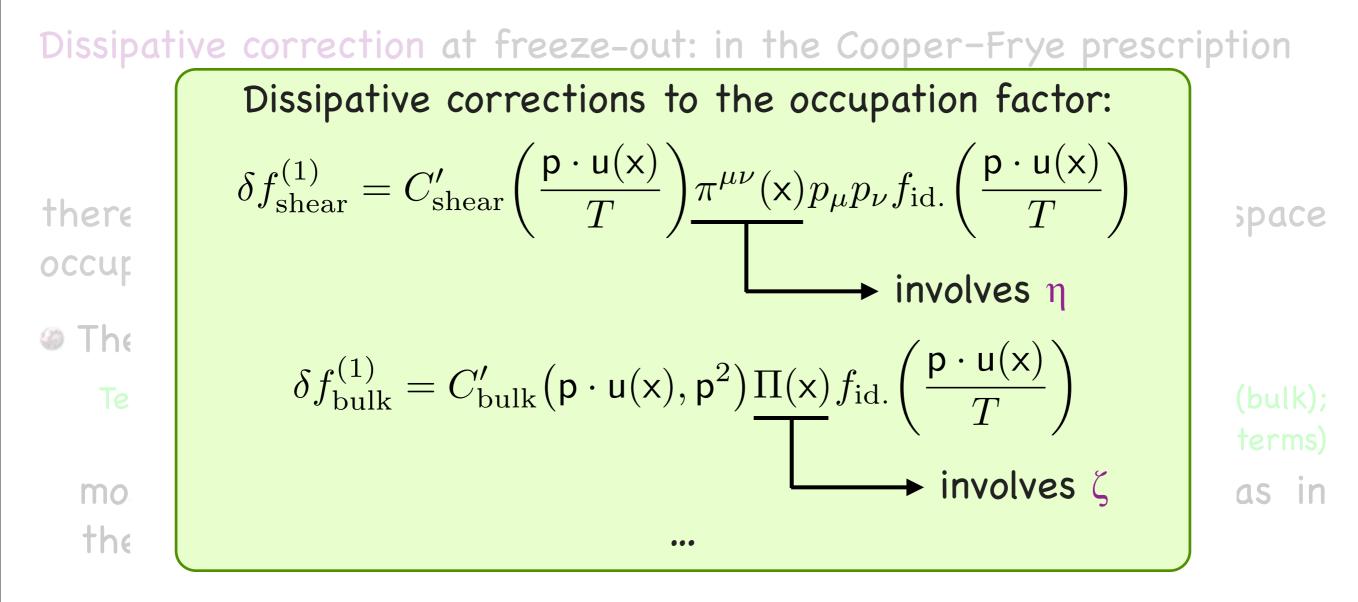
r (as yet) unknown functional dependences  $\eta(T)$ ,  $\zeta(T)$ ,  $\kappa(T)$ ...

Dissipative correction at freeze-out: in the Cooper-Frye prescription

$$E_{\vec{p}} \frac{\mathrm{d}^3 N}{\mathrm{d}^3 \vec{p}} = \frac{g}{(2\pi)^3} \int_{\Sigma} f\left(\frac{\mathbf{p} \cdot \mathbf{u}(\mathbf{x})}{T}\right) \mathbf{p} \cdot \mathrm{d}^3 \sigma(\mathbf{x})$$

there come corrections  $f = f_{id.} + \delta f^{(1)} + \delta f^{(2)} + \cdots$  to the phase space occupation factor.

The functional form of the corrections has been computed Teaney 2003 (shear); Dusling & Teaney, Denicol et al., Monnai & Hirano 2008- (bulk); Teaney & Yan 2013 (conformal 2nd order terms) mostly assuming freeze-out to a simple-component kinetic gas in the relaxation time approximation.



Dissipative correction at freeze-out: in the Cooper-Frye prescription

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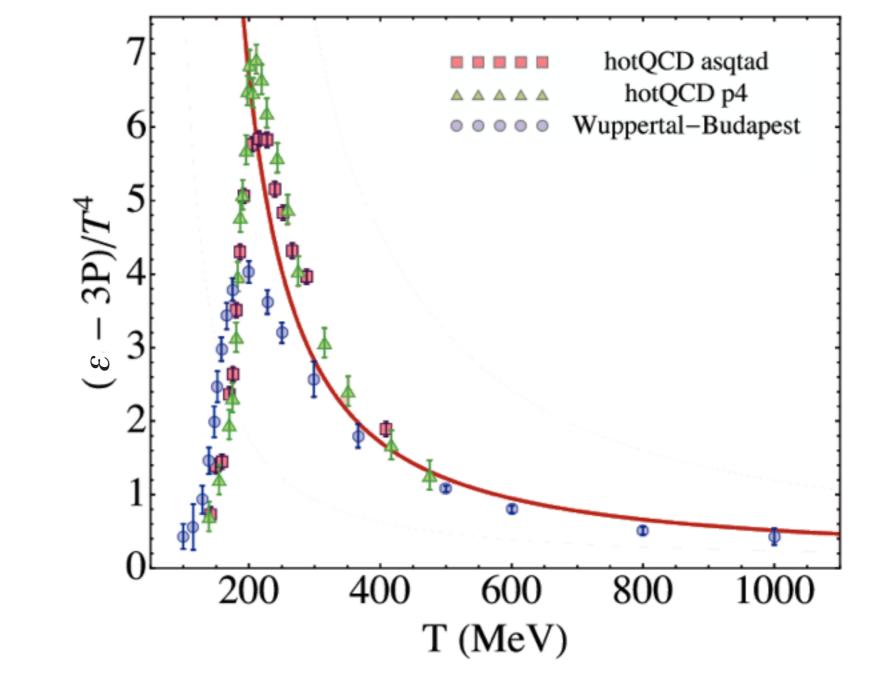
 Teaney known.

Only the values of the transport coefficients at freeze-out matter.

For if freeze-out at some temperature  $T_{\text{f.o.}}$ , only  $\eta(T_{\text{f.o.}})$ ,  $\zeta(T_{\text{f.o.}})$ ...

#### Dissipative corrections at freeze-out

If  $T_{f.o} < T_c$ , the decoupling fluid is to a good approximation conformal:



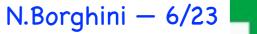
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Dissipative effects in heavy ion collisions

#### Principle and ideas of the calculations

Results

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#### Particle emission at freeze-out

Consider the Cooper-Frye formula (T is the freeze-out temperature)

$$E_{\vec{p}} \frac{\mathrm{d}^3 N}{\mathrm{d}^3 \vec{p}} = \frac{g}{(2\pi)^3} \int_{\Sigma} f\left(\frac{\mathbf{p} \cdot \mathbf{u}(\mathbf{x})}{T}\right) \mathbf{p} \cdot \mathrm{d}^3 \sigma(\mathbf{x})$$

The phase space occupation factor f is proportional to  $f_{id.}$ , which will be approximated by a Maxwell-Boltzmann distribution.

The integral can be computed with the saddle-point approximation, without needing any detail on the freeze-out surface  $\Sigma$ .

( $\mathbb{C}$  the ensuing results are thus to a large extent irrespective of the velocity profile, i.e. of whether u(x) is a solution to ideal or dissipative fluid dynamics)

row one needs to determine the saddle point, which is the minimum of  $p \cdot u(x)/T$ .

\* at least approximately

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#### Particle emission at freeze-out

Taking the Cooper-Frye formula seriously

$$E_{\vec{p}} \frac{\mathrm{d}^3 N}{\mathrm{d}^3 \vec{p}} = \frac{g}{(2\pi)^3} \int_{\Sigma} f\left(\frac{\mathbf{p} \cdot \mathbf{u}(\mathbf{x})}{T}\right) \mathbf{p} \cdot \mathrm{d}^3 \sigma(\mathbf{x})$$

one may approximate the integral using the steepest-descent method. N.B. & J.-Y.Ollitrault 2005

Two categories of particles:

Some point on  $\Sigma$ .

► at a given rapidity y, 
$$|\mathbf{p}_t| < m u_{\max}(y)$$
.  
► maximum fluid velocity  
in the direction of  $p^{\mu}$ 

The minimum value of  $p \cdot u(x)/T$  simply equals m/T, independent of the particle momentum.

#### Particle emission at freeze-out

Taking the Cooper-Frye formula seriously

$$E_{\vec{p}} \frac{\mathrm{d}^3 N}{\mathrm{d}^3 \vec{p}} = \frac{g}{(2\pi)^3} \int_{\Sigma} f\left(\frac{\mathbf{p} \cdot \mathbf{u}(\mathbf{x})}{T}\right) \mathbf{p} \cdot \mathrm{d}^3 \sigma(\mathbf{x})$$

one may approximate the integral using the steepest-descent method. N.B. & J.-Y.Ollitrault 2005

Two categories of particles:

Some point on  $\Sigma$ .

► at a given rapidity y,  $|\mathbf{p}_t| < m u_{\max}(\mathbf{y})$ . The direction of  $p^{\mu}$ 

• "fast particles":  $|\mathbf{p}_t| > mu_{\max}(\mathbf{y})$ . The minimum value of  $\mathbf{p} \cdot \mathbf{u}(\mathbf{x})/T$  is larger than m/T.

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#### Results for slow particles

"Slow particles": emitted by fluid cells w.r.t. which they are at rest. Velocity  $\frac{p}{m}$  coincides with that of the fluid u(x) at the saddle point.

Freezing out from an ideal fluid:

The Cooper-Frye integral 
$$E_{\vec{p}} \frac{\mathrm{d}^3 N}{\mathrm{d}^3 \vec{p}} = \frac{g}{(2\pi)^3} \int_{\Sigma} f_{\mathrm{id.}} \left( \frac{\mathsf{p} \cdot \mathsf{u}(\mathsf{x})}{T} \right) \mathsf{p} \cdot \mathrm{d}^3 \sigma(\mathsf{x})$$

yields a function of the particle velocity only, with an m-dependent prefactor:

$$E_{\vec{p}} \frac{\mathrm{d}^3 N}{\mathrm{d}^3 \vec{p}} = C(m) F\left(\frac{\mathbf{p}_t}{m}, \mathbf{y}\right)$$

Fourier-expanding, the flow coefficients  $v_n$  for all particles coincide when considered at the same transverse velocity and rapidity.

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N.B. & J.-Y.Ollitrault 2005

#### Results for slow particles

Particles with velocity  $\frac{p}{m}$  are all emitted from the same saddle point.

Freezing out from a dissipative fluid:

Considering first order only, the Cooper-Frye integral again gives an m-dependent pre factor times a function of the particle velocity.

$$E_{\vec{p}} \frac{\mathrm{d}^3 N}{\mathrm{d}^3 \vec{p}} = C'(m) F'\left(\frac{\mathbf{p}_t}{m}, \mathbf{y}\right)$$

 $\Rightarrow$  mass-scaling of anisotropic flow persists

Proof:

• Since the saddle point obeys  $u^{\mu}(\mathbf{x}) = p^{\mu}/m$ , the shear term vanishes

$$\delta f_{\text{shear}}^{(1)} = C_{\text{shear}}' \left( \frac{\mathsf{p} \cdot \mathsf{u}(\mathsf{x})}{T} \right) \pi^{\mu\nu}(\mathsf{x}) p_{\mu} p_{\nu} f_{\text{id.}} \left( \frac{\mathsf{p} \cdot \mathsf{u}(\mathsf{x})}{T} \right) \text{ with } p^{\mu} p^{\nu} \pi_{\mu\nu} = \mathbf{0}$$

• For the bulk viscosity term, use the "universality" of the saddle point

#### Fast particles

Fast particles emitted in a given direction come from the same saddle point, where the fluid has velocity  $u_{\max}(y, \varphi)$ .

At the saddle point,  $\mathbf{p} \cdot \mathbf{u}(\mathbf{x}) = m_t u_{\max}^0(y, \varphi) - p_t u_{\max}(y, \varphi)$ , with here  $u_{\max}^0 \equiv \sqrt{1 + u_{\max}^2}$ .

**w** governs the particle spectrum.

As a second step, write

$$u_{\max}(y,\varphi) = \bar{u}_{\max}(y) \left[ 1 + 2\sum_{n\geq 1} V_n(y) \cos n(\varphi - \Psi_n) \right]$$

and Taylor-expand (with respect to the small coefficients  $V_n$ ) to find the flow coefficients  $v_n(p_t, y)$ .

## Fast particles from an ideal fluid

Reasonable(?) assumption: the velocity of the freezing-out fluid mostly has elliptic and triangular anisotropies:  $V_2$ ,  $V_3 \gg V_1$ ,  $V_4$ ,  $V_5$ ,  $V_6$ 

One then finds

$$v_2(p_t) = I(p_t)V_2$$

 $v_3(p_t) = I(p_t)V_3$ •  $v_4(p_t) = \frac{I(p_t)^2}{2}V_2^2 + I(p_t)V_4$  $v_5(p_t) = I(p_t)^2 V_2 V_3 + I(p_t) V_5$ •  $v_6(p_t) = \frac{I(p_t)^3}{\epsilon}V_2^3 + \frac{I(p_t)^2}{2}V_3^2 + I(p_t)^2V_2V_4 + I(p_t)V_6$ where  $I(p_t) \equiv \frac{\bar{u}_{\max}}{T}(p_t - m_t \bar{v}_{\max})$  with  $\bar{v}_{\max} \equiv \frac{u_{\max}}{\sqrt{1 + \bar{u}_{\max}^2}}$ N.B. & J.-Y.Ollitrault 2005; D.Teaney & L.Yan 2012

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Reasonable(?) assumption: the velocity of the freezing-out fluid mostly has elliptic and triangular anisotropies:  $V_2$ ,  $V_3 \gg V_1$ ,  $V_4$ ,  $V_5$ ,  $V_6$ 

One then finds at high momentum (not too high, hydro should hold!)

$$v_2(p_t) = I(p_t)V_2$$

 $v_3(p_t) = I(p_t)V_3$ •  $v_4(p_t) = \frac{I(p_t)^2}{2}V_2^2 + I(p_t)V_4 \sim \frac{1}{2}v_2(p_t)^2$ •  $v_5(p_t) = I(p_t)^2 V_2 V_3 + I(p_t) V_5 \sim v_2(p_t) v_3(p_t)$ •  $v_6(p_t) = \frac{I(p_t)^3}{6}V_2^3 + \frac{I(p_t)^2}{2}V_3^2 + \sim (\frac{1}{6}v_2(p_t)^3 + \frac{1}{2}v_3(p_t)^2)$ where  $I(p_t) \equiv \frac{\bar{u}_{\max}}{T}(p_t - m_t \bar{v}_{\max})$  with  $\bar{v}_{\max} \equiv \frac{u_{\max}}{\sqrt{1 + \bar{u}_{\max}^2}}$ N.B. & J.-Y.Ollitrault 2005; D.Teaney & L.Yan 2012

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Assumptions:  $V_2$ ,  $V_3 \gg V_1$ ,  $V_4$ ,  $V_5$ ,  $V_6$  & azimuthal dependence of the shear part of the stress tensor is neglected (for the sake of simplicity only).

Remarks:

- Strictly speaking, the values of these Fourier coefficients, as well as that of  $\bar{u}_{\max}$  (which enters the function  $I(p_t)$ ) are different from those of the ideal case.
- Hereafter I only mention the correction due to shear viscosity. That arising from bulk viscosity and those from second order terms lead to similar results.

Assumptions:  $V_2$ ,  $V_3 \gg V_1$ ,  $V_4$ ,  $V_5$ ,  $V_6$  & azimuthal dependence of the shear part of the stress tensor is neglected (for the sake of simplicity only).

One then finds

• 
$$v_2(p_t) = [I(p_t) - D(p_t)]V_2$$
  
•  $v_3(p_t) = [I(p_t) - D(p_t)]V_3$   
•  $v_4(p_t) = \left[\frac{I(p_t)^2}{2} - I(p_t)D(p_t)\right]V_2^2 + [I(p_t) - D(p_t)]V_4$   
•  $v_5(p_t) = [I(p_t)^2 - I(p_t)D(p_t)]V_2V_3 + [I(p_t) - D(p_t)]V_5$   
•  $v_6(p_t) = \left[\frac{I(p_t)^3}{6} - \frac{I(p_t)^2D(p_t)}{2}\right]V_2^3 + \left[\frac{I(p_t)^2}{2} - I(p_t)D(p_t)\right]V_3^2 + \cdots$ 

where  $D(p_t)$  is a positive function proportional to  $\eta$ , whose functional dependence reflects that of the viscous correction  $\delta f_{\rm shear}^{(1)}$ .

Assumptions:  $V_2$ ,  $V_3 \gg V_1$ ,  $V_4$ ,  $V_5$ ,  $V_6$  & azimuthal dependence of the shear part of the stress tensor is neglected (for the sake of simplicity only).

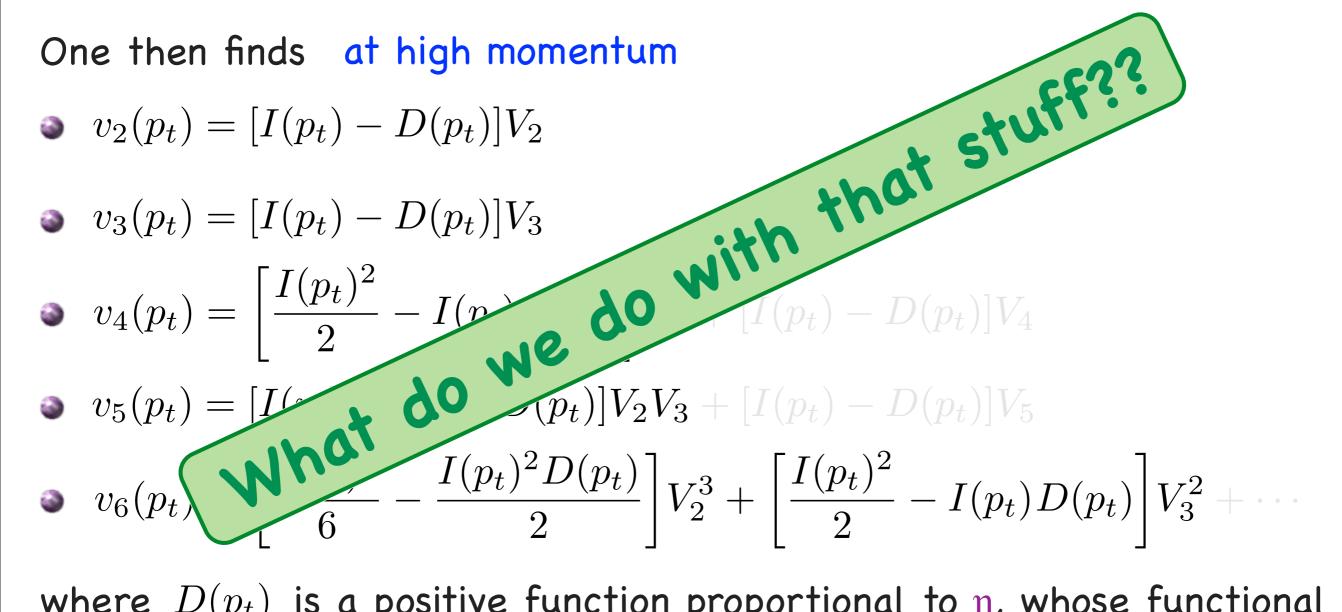
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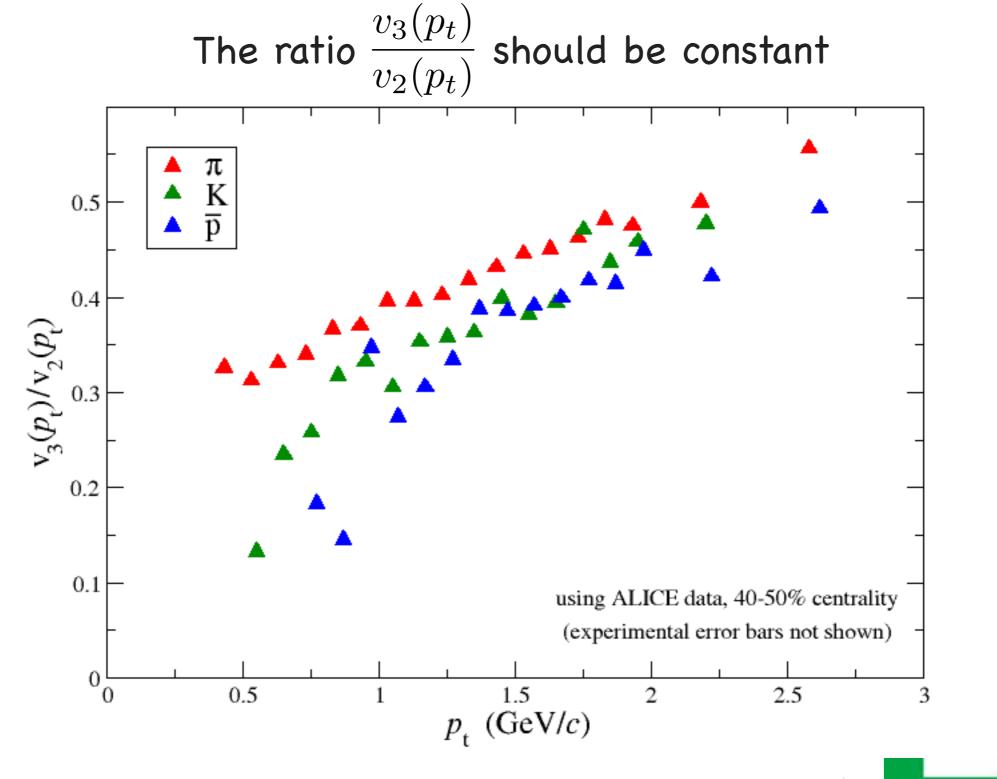
Inspecting these results more carefully...

• 
$$v_2(p_t) = [I(p_t) - D(p_t)]V_2$$
  
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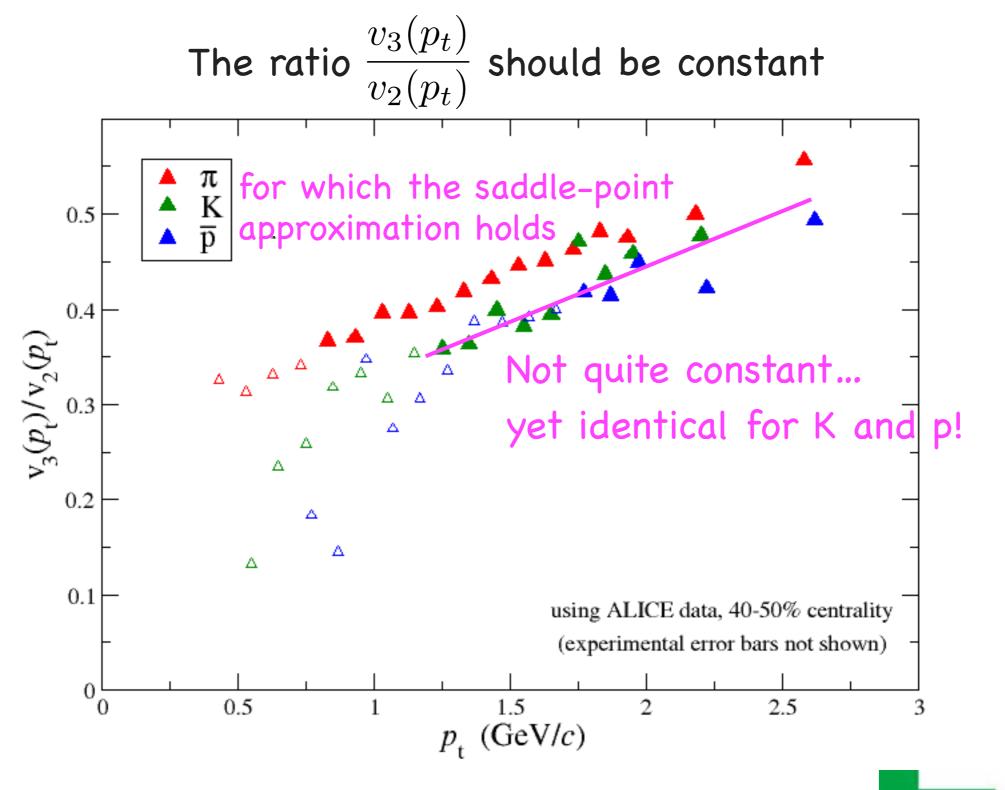
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•  $v_3(p_t) = [I(p_t) - D(p_t)]V_3$   
• the ratio  $\frac{v_3(p_t)}{v_2(p_t)}$  should be constant  
•  $v_4(p_t) = \left[\frac{I(p_t)^2}{2} - I(p_t)D(p_t)\right]V_2^2 + [I(p_t) - D(p_t)]V_4$   
•  $v_5(p_t) = [I(p_t)^2 - I(p_t)D(p_t)]V_2V_3 + [I(p_t) - D(p_t)]V_5$   
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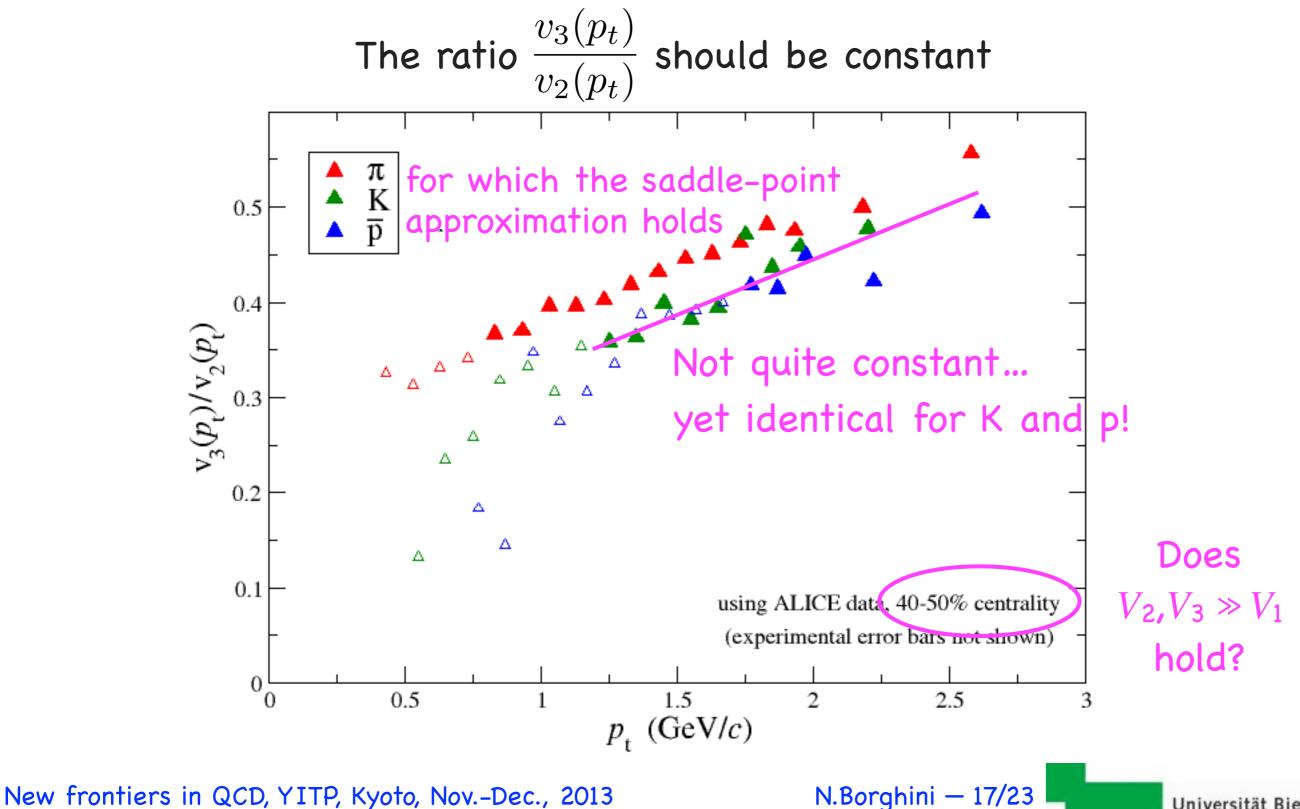
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The ratio  $rac{v_3(p_t)}{v_2(p_t)}$  should be constant

Actually,

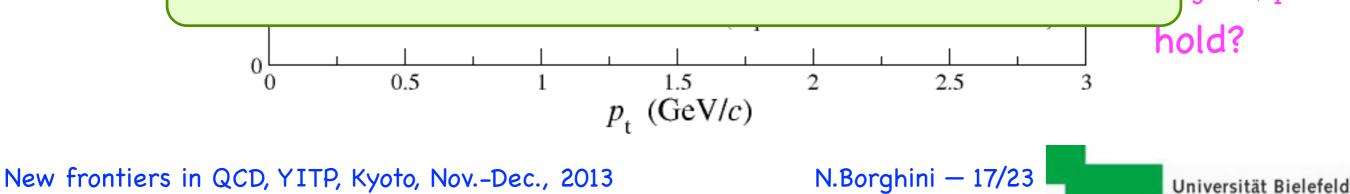
$$v_3(p_t) = [I(p_t) - D(p_t)]V_3 + [I(p_t)^2 - I(p_t)D(p_t)]V_1V_2$$

Thus  

$$\frac{v_3(p_t)}{v_2(p_t)} = \frac{V_3}{V_2} + I(p_t)V_1 \simeq \frac{V_3}{V_2} + \underbrace{v_1(p_t)}_{V_1}$$
linear(?)

which might explain the data...

But no identified  $v_1(p_t)$  is available yet.



Inspecting the results more carefully...

• 
$$v_2(p_t) = [I(p_t) - D(p_t)]V_2$$

•  $v_3(p_t) = [I(p_t) - D(p_t)]V_3$ 

• 
$$v_4(p_t) = \left[\frac{I(p_t)^2}{2} - I(p_t)D(p_t)\right]V_2^2 < \frac{1}{2}v_2(p_t)^2$$

• 
$$v_5(p_t) = [I(p_t)^2 - I(p_t)D(p_t)]V_2V_3 + [as_{p_t}seen_{lin_p_t}ransport and$$
  
•  $v_6(p_t) = \left[\frac{I(p_t)^3}{6} - \frac{I(p_t)^2D(p_t)}{2}\right]V_2^3 + \left[\frac{I(p_t)^2}{2} - I(p_t)D(p_t)\right]V_3^2 + \cdots$ 

Inspecting the results more carefully...

• 
$$v_2(p_t) = [I(p_t) - D(p_t)]V_2$$

• 
$$v_3(p_t) = [I(p_t) - D(p_t)]V_3$$

- $v_4(p_t) = \left| \frac{I(p_t)^2}{2} I(p_t)D(p_t) \right| V_2^2 + [I(p_t) D(p_t)]V_4$
- $v_5(p_t) = [I(p_t)^2 I(p_t)D(p_t)]V_2V_3 > v_2(p_t)v_3(p_t)$

as seen in (real) hydro simulations (I use  $I(p_t) > D(p_t)$ )

Inspecting the results more carefully...

• 
$$v_2(p_t) = [I(p_t) - D(p_t)]V_2$$

• 
$$v_3(p_t) = [I(p_t) - D(p_t)]V_3$$

- together  $\left| \begin{array}{c} I(p_t)^2 \\ \text{with} \\ 2 \end{array} I(p_t) D(p_t) \right| V_2^2 + [I(p_t) D(p_t)] V_4$
- $v_5(p_t) = [I(p_t)^2 I(p_t)D(p_t)]V_2V_3 + [I(p_t) D(p_t)]V_5$

yield 
$$\frac{v_5(p_t) - v_2(p_t)v_3(p_t)}{v_2(p_t)} = D(p_t)V_3$$

i.e. isolate the dissipative contribution to  $v_3(p_t)$ .

Inspecting the results more carefully...

• 
$$v_2(p_t) = [I(p_t) - D(p_t)]V_2$$

• and 
$$t = [I(p_t) - D(p_t)]V_3$$
  
•  $v_4(p_t) = \left[\frac{I(p_t)^2}{2} - I(p_t)D(p_t)\right]V_2^2 + [I(p_t) - D(p_t)]V_4$ 

•  $v_5(p_t) = [I(p_t)^2 - I(p_t)D(p_t)]V_2V_3 + [I(p_t) - D(p_t)]V_5$ 

yield  $2v_4(p_t) - v_2(p_t)^2 = -D(p_t)^2 V_2^2$ 

i.e. again isolate the dissipative contribution (here to  $v_2(p_t)$ ).

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More relations can be found...

For instance, combining

$$\frac{v_5(p_t) - v_2(p_t)v_3(p_t)}{v_3(p_t)} = D(p_t)V_2$$

(analogous to the relation on slide 20) and

$$2v_4(p_t) - v_2(p_t)^2 = -D(p_t)^2 V_2^2$$

one at once comes up with a relation between four harmonics...

... up to the caveats on my summary slide!

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Viscosity and other dissipative phenomena strike twice: throughout the evolution and at freeze-out

Their contributions at freeze-out might be isolated

relations between various flow harmonics (for a given particle species)

(similar relations with multiparticle correlations; not shown here)

hope (naïve?): using particles which decouple earlier / later, one may access the temperature dependence of the transport coefs.

#### Caveats:

- Throughout this talk, fluctuations were neglected (not a big deal)
- How much of these ideas survives: 1. real hydro; 2. rescatterings realistic studies needed!